(19) World Intellectual Property Organization International Bureau



(43) International Publication Date 24 April 2003 (24.04.2003)

PCT

(10) International Publication Number WO 03/033138 A1

(51) International Patent Classification⁷: 23/52, C07C 51/25, 51/215

B01J 23/68,

(21) International Application Number: PCT/GB02/04018

_

(22) International Filing Date:

4 September 2002 (04.09.2002)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

0124835.0

16 October 2001 (16.10.2001) GB

0218870.4

13 August 2002 (13.08.2002) GI

(71) Applicant (for all designated States except US): BP CHEMICALS LIMITED [GB/GB]; Britannic House, 1 Finsbury Circus, London EC2M 7BA (GB).

(72) Inventor; and

(75) Inventor/Applicant (for US only): ELLIS, Brian [GB/GB]; 38 Hawkewood Road, Lower Sunbury, Middlesex TW16 6HJ (GB).

(74) Agent: BROOKE, Caron; BP International Limited, Patents & Agreements, Chertsey Road, Sunbury on Thames, Middlesex TW16 7LN (GB).

(81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW,

MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

(84) Designated States (regional): ARIPO patent (GH, GM, KE, LS, MW, MZ, SI), SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, Fl, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Declarations under Rule 4.17:

- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii)) for the following designations AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, VN, YU, ZA, ZM, ZW, ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG)
- of inventorship (Rule 4.17(iv)) for US only

Published:

-- with international search report

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: ETHANE OXIDATION CATALYST AND PROCESS UTILISING THE CATALYST

(57) Abstract: A catalyst composition and its use for the selective oxidation of ethane to acetic acid and/or for the selective oxidation of ethylene to acetic acid which composition comprises in combination with oxygen the elements molybdenum, vanadium, niobium, gold in the absence of palladium according to the empirical formula: $Mo_aW_bAu_cV_dNb_cZ_f$ wherein Z is one or more elements selected from the group consisting of B, A1, Ga, In, Ge, Sn, Pb, Sb, Cu, Pt, Ag, Fe and Re; a, b, c, d, e and f represent the gram atom ratios of the elements such that: $0 < a \le 1$; $0 \le b < 1$ and a + b = 1; $10^{-5} \varphi c \le 0.02$; $0 < d \le 2$; $0 < e \le 1$; and $0.0001 \le f \le 0.05$.



5

10

15

20

ETHANE OXIDATION CATALYST AND PROCESS UTILISING THE CATALYST

The present invention relates to a catalyst for the selective oxidation of ethane to acetic acid and/or for the selective oxidation of ethylene to acetic acid, and to a process for the production of acetic acid utilising the aforesaid catalyst.

Catalysts comprising molybdenum, vanadium and niobium in combination with oxygen for use in processes for the production of acetic acid by the oxidation of ethane and ethylene are known in the art from, for example, US 4,250,346, EP-A-1043064, WO 99/20592 and DE 196 30 832.

US Patent No. 4,250,346 discloses the oxidative dehydrogenation of ethane to ethylene in a gas phase reaction at relatively high levels of conversion, selectivity and productivity to ethylene at a temperature of less than about 550°C using as a catalyst a composition comprising the elements molybdenum, X and Y in the ratio Mo_aX_bY_c wherein X is Cr, Mn, Nb, Ta, Ti, V and/or W, and preferably Mn, Nb, V and/or W; Y is Bi, Ce, Co, Cu, Fe, K, Mg, Ni, P, Pb, Sb, Si, Sn, Tl and/or U, and preferably Sb, Ce and/or U, a is 1, b is 0.05 to 1.0 and c is 0 to 2, and preferably 0.05 to 1.0, with the proviso that the total value of c for Co, Ni and/or Fe is less than 0.5.

WO 99/20592 relates to a method of selectively producing acetic acid from ethane, ethylene or mixtures thereof and oxygen at high temperature in the presence of a catalyst having the formula $Mo_aPd_bX_cY_d$ wherein X represents one or several of Cr, Mn, Nb, Ta, Ti, V, Te and W; Y represents one or several of B, Al, Ga, In, Pt, Zn, Cd, Bi, Ce, Co, Rh, Ir, Cu, Ag, Au, Fe, Ru, Os, K, Rb, Cs, Mg, Ca, Sr, Ba, Nb, Zr, Hf, Ni, P, Pb, Sb, Si, Sn, Tl and U and a=1, b=0.0001 to 0.01, c = 0.4 to 1 and d = 0.005 to 1.

German patent application DE 196 30 832 A1 relates to a similar catalyst

composition in which a = 1, b > 0, c > 0 and d = 0 to 2. Preferably, a = 1, b = 0.0001 to 0.5, c = 0.1 to 1.0 and d = 0 to 1.0.

The catalysts of both WO 99/20592 and DE 19630832 require the presence of palladium.

EP-A-1043064 discloses a catalyst composition for the oxidation of ethane to ethylene and/or acetic acid and/or for the oxidation of ethylene to acetic acid which comprises in combination with oxygen the elements molybdenum, vanadium, niobium and gold in the absence of palladium according to the empirical formula:

 $Mo_aW_bAu_cV_dNb_eY_f$ (I)

5

10

15

20

25

30

wherein Y is one or more elements selected from the group consisting of : Cr, Mn, Ta, Ti, B, Al, Ga, In, Pt, Zn, Cd, Bi, Ce, Co, Rh, Ir, Cu, Ag, Fe, Ru, Os, K, Rb, Cs, Mg, Ca, Sr, Ba, Zr, Hf, Ni, P, Pb, Sb, Si, Sn, Tl, U, Re, Te, La and Pd; a, b, c, d, e and f represent the gram atom ratios of the elements such that : $0 < a \le 1$; $0 \le b < 1$ and a + b = 1; $10^{-5} < c \le 0.02$; $0 < d \le 2$; $0 < e \le 1$; and $0 \le f \le 2$.

There remains a need to develop a catalyst for the oxidation of ethane and/or ethylene to acetic acid and a process for the production of acetic acid using said catalyst and wherein the catalyst enables a high selectivity to acetic acid to be achieved.

Surprisingly, it has now been found that it is possible by using a catalyst that contains, in combination with oxygen, the elements molybdenum, vanadium, niobium and gold and one or more elements selected from the group consisting of boron, aluminium, gallium, indium, germanium, tin, lead, antimony, copper, platinum, silver, iron and rhenium, in the absence of palladium, to oxidise ethane and/or ethylene to acetic acid with a high selectivity to acetic acid. Furthermore, it has been found possible using the catalysts of the present invention, to achieve a high selectivity to acetic acid with reduced, for example, little, if any, selectivity to ethylene.

Accordingly, the present invention provides a catalyst composition for the selective oxidation of ethane to acetic acid and/or for the selective oxidation of ethylene to acetic acid which composition comprises in combination with oxygen the elements molybdenum, vanadium, niobium, gold in the absence of palladium according to the empirical formula: Mo_aW_bAu_cV_dNb_eZ_f (I) wherein Z is one or more elements selected from the group consisting of B, Al, Ga, In, Ge, Sn, Pb, Sb, Cu, Pt, Ag, Fe and Re;

5

20

25

30

a, b, c, d, e and f represent the gram atom ratios of the elements such that:

 $0 < a \le 1$; $0 \le b < 1$ and a + b = 1; $10^{-5} < c \le 0.02$; $0 < d \le 2$; $0 < e \le 1$; and $0.0001 \le f \le 0.05$

Catalysts embraced within the formula (I) include:-

 $Mo_aW_bAu_cV_dNb_eSn_f$

 $Mo_a.Au_cV_dNb_eSn_f$

Preferably, Z is Sn, Ag, Fe or Re, especially Sn.

Examples of suitable catalysts having the formula (I) include:-

 $Mo_{1.000} V_{0.423} Nb_{0.115} Au_{0.008} Ag_{0.008} O_y$

Mo1.000 V_{0.423} Nb_{0.115} Au_{0.008} Fe_{0.0156} O_y,

Mo_{1.000} V_{0.423} Nb_{0.115} Au_{0.008} Re_{0.008} O_y,

 $Mo_{1.00}V_{0.423}Nb_{0.115}Au_{0.0008}Sn_{0.0008}O_y$, and

 $Mo_{1.00}V_{0.423}Nb_{0.117}Au_{0.0008}Sn_{0.0156}O_y$, wherein y is a number which satisfies the valencies of the elements in the composition for oxygen.

 $\begin{aligned} &\text{Preferably } 0.01 < a \leq 1. \text{ Preferably, } 0.1 < d \leq 2. \text{ Preferably, } 0.01 < e \leq 0.5, \text{ for } \\ &\text{example, } 0.05 \leq e \leq 0.15. \text{ Preferably, } 0.0005 \leq f \leq 0.02. \end{aligned}$

An advantage of the catalyst compositions of the present invention is that they are highly selective in converting ethane and/or ethylene to acetic acid. Typically, using the catalyst compositions of the present invention, a selectivity to acetic acid of at least 50mol%, preferably at least 60mol%, such as at least 70mol%, may be achieved.

In particular, using the catalyst compositions of the present invention, a high selectivity to acetic acid may be achieved in combination with a low, if any, selectivity to ethylene.

Typically, using the catalyst compositions of the present invention, the selectivity to ethylene is less than 25 mol%, preferably, less than 10 mol%, such as less than 5 mol%.

Preferably, using the catalyst compositions of the present invention, the selectivity to acetic acid is at least 60mol%, such as at least 70mol% and the selectivity to ethylene is less than 15mol%, such as less than 10 mol%.

As used herein, selectivity refers to a percentage that reflects the amount of desired acetic acid product produced as compared to the total carbon in the products formed:-

% selectivity = 100 * Moles of acetic acid produced / S

5

10

15

20

25

30

wherein S = the molar acid-equivalent sum (carbon basis) of all carbon-containing products, excluding the alkane in the effluent

The catalyst compositions may be prepared by any of the methods conventionally employed for the preparation of catalysts. Suitably the catalyst may be prepared from a solution of soluble compounds and/or complexes and/or compounds of each of the metals. The solution is preferably an aqueous system having a pH in the range from 1 to 12, preferably from 2 to 8, at a temperature of from 20° to 100°C.

Generally, a mixture of compounds containing the elements is prepared by dissolving sufficient quantities of soluble compounds and dispersing any insoluble compounds so as to provide a desired gram-atom ratio of the elements in the catalyst composition. The catalyst composition may then be prepared by removing the solvent from the mixture. The catalyst may be calcined by heating to a temperature of from 200 to 550°C, suitably in air or oxygen, for a period of from 1 minute to 24 hours. Preferably, the air or oxygen is slowly flowing.

The catalyst may be used unsupported or supported. Suitable supports include silica, alumina, zirconia, titania, silicon carbide and mixtures of two or more thereof.

Further details of a suitable method for preparing a catalyst composition may be found in, for example, EP-A-0166438.

The catalyst may be used in the form of a fixed or a fluidised bed.

In another embodiment the present invention provides a process for the selective production of acetic acid from a gaseous mixture comprising ethane and/or ethylene which process comprises contacting the gaseous mixture with a molecular oxygen-containing gas at elevated temperature in the presence of a catalyst composition as hereinbefore described.

Ethane is selectively oxidised to acetic acid and/or ethylene is selectively oxidised to acetic acid. Preferably, ethane and optionally ethylene is oxidised to a mixture comprising acetic acid which may be used with or without the addition or removal of acetic acid for the production of vinyl acetate by reaction with a molecular

oxygen-containing gas in an integrated process.

5

10

15

20

25

30

The feed gas comprises ethane and/or ethylene, preferably ethane.

Ethane and/or ethylene may be used in substantially pure form or admixed with one or more of nitrogen, methane, carbon dioxide and water in the form of steam, which may be present in major amounts, for example greater than 5 volume percent or one or more of hydrogen, carbon monoxide, C₃/C₄ alkenes and alkenes, which may be present in minor amounts, for example less than 5 volume percent.

The molecular oxygen-containing gas may be air or a gas richer or poorer in molecular oxygen than air, for example oxygen. A suitable gas may be, for example, oxygen diluted with a suitable diluent, for example nitrogen.

It is preferred to feed, in addition to ethane and/or ethylene and the molecular oxygen-containing gas, water (steam) because this can improve the selectivity to acetic acid.

The elevated temperature may suitably be in the range from 200 to 500°C, preferably from 200 to 400°C.

The pressure may suitably be atmospheric or superatmospheric, for example in the range from 1 to 50 bar, preferably from 1 to 30 bar.

The catalyst composition is preferably calcined before use in the process of the invention. Calcination may suitably be achieved by heating at a temperature suitably in the range from 250 to 500°C in the presence of an oxygen-containing gas, for example air.

Operating conditions and other information applicable to the performance of the invention may be found in the aforesaid prior art, for example US Patent No. 4,250,346.

The process of the invention will now be further illustrated by reference to the following Examples.

CATALYST PREPARATION

Preparation of Catalyst A (Comparative)

A solution 'A' was prepared by dissolving 22.935 g of ammonium molybdate and 0.0357 g of ammonium gold chloride in 100 ml of distilled water at 70°C with stirring. A solution 'B' was prepared by dissolving 6.434 g of ammonium vanadate in 150 ml of distilled water at 70°C with stirring. A solution 'C' was prepared by dissolving 7.785 g of ammonium niobium oxalate in 100 ml of distilled water at 70°C

5

10

20

25

30

ł

with stirring. Each of the solutions A, B and C was left for 15 minutes to allow maximum solubilisation of the components. Solution C was then added to solution B rapidly with stirring at 70°C. The mixed solution B/C was stirred for 15 minutes at 70°C then added rapidly to solution A. The final mixed solution A/B/C was left to stir at 70°C for a further 15 minutes, after which the solution was heated to boiling to facilitate evaporation of the water. Full evaporation of the reactant mixture was achieved in 1.5 hours, resulting in a dry paste. The beaker with the dried paste was then transferred to an oven for further drying at 120°C for 2 hours. After drying, the catalyst precursor was ground to a fine powder and then sieved through a 0.2 mm mesh sieve. The resulting powdered catalyst cake was then calcined in static air in an oven at 400°C for 4 hours. The nominal formula of the oxide catalyst obtained was:

 $Mo_{1.000}\,V_{0.423}\;Nb_{0.115}\,Au_{0.0008}\,Oy$

This catalyst is not a catalyst according to the invention because it contains no element from the group consisting of B, Al, Ga, In, Ge, Sn, Pb, Sb, Cu, Pt, Ag, Fe and Re.

Preparation of Catalyst B

A catalyst B was prepared as for catalyst A except that 0.0190 g of tin (II) chloride was additionally added to solution A. The nominal formula of the oxide catalyst obtained was:

 $Mo_{1.000}\,V_{0.423}\,Nb_{0.115}\,Au_{0.0008}\,Sn_{0.0008}\,O_y$

Preparation of Catalyst C

A catalyst C was prepared as for catalyst A except that 0.3792 g of tin (II) chloride was added to solution A. The nominal formula of the oxide catalyst obtained was:

 $Mo_{1.000}\,V_{0.423}\;Nb_{0.117}\;Au_{0.0008}\;Sn_{0.0156}\,O_y$

Preparation of catalyst D

A catalyst D was prepared as for catalyst A but with addition of 0.0299 g of antimony (III) acetate (FW 298.88) to solution A. The nominal formula of the oxide catalyst was thus:

 $Mo_{1.000}\,V_{0.423}\;Nb_{0.115}\;Au_{0.008}\;Sb_{0.008}\;O_y$

Preparation of catalyst E

A catalyst E was prepared as for catalyst A but with addition of 0.0200 g of copper (II) acetate (FW 199.65) to solution A. The nominal formula of the oxide catalyst was thus:

Mo_{1.000} V_{0.423} Nb_{0.115} Au_{0.008} Cu_{0.008} O_y

5 Preparation of catalyst F

A catalyst F was prepared as for catalyst A but with addition of 0.0027 g of platinum acetate (FW 352.66) to solution A. The nominal formula of the oxide catalyst was thus:

Mo_{1.000} V_{0.423} Nb_{0.115} Au_{0.008} Pt _{0.0006} O_y

10 Preparation of catalyst G

A catalyst G was prepared as for catalyst A but with addition of 0.0174 g of silver (I) acetate (FW 166.92) to solution A. The nominal formula of the oxide catalyst was thus:

Mo_{1.000} V_{0.423} Nb_{0.115} Au_{0.008} Ag_{0.008} O_y

15 Preparation of catalyst H

A catalyst H was prepared as for catalyst A but with addition of 0.8080 g of ferric (III) nitrate (FW 404.00) to solution A. The nominal formula of the oxide catalyst was thus:

 $Mo_{1.000}\,V_{0.423}\,Nb_{0.115}\,Au_{0.008}\,Fe_{0.0156}\,O_y$

20 Preparation of catalyst I

A catalyst I was prepared as for catalyst A but with addition of 0.0268 g of ammonium rhenate (FW 268.24) to solution A. The nominal formula of the oxide catalyst was thus:

 $Mo_{1.000}\,V_{0.423}\,Nb_{0.115}\,Au_{0.008}\,Re_{0.008}\,O_y$

25 <u>Preparation of catalyst J</u>

A catalyst J was prepared as for catalyst A but with addition of 0.0256 g of gallium nitrate (FW 255.74) to solution A. The nominal formula of the oxide catalyst was thus:

 $Mo_{1.000}\,V_{0.423}\,Nb_{0.115}\,Au_{0.008}\,Ga_{0.008}\,O_y$

30 General Ethane Oxidation Reaction Method

Typically 5 ml of a powdered catalyst A to J was mixed with 15 ml of glass beads of diameter 0.4 mm to form a diluted catalyst bed of 20 ml in volume. The diluted

catalyst was then loaded into a fixed bed reactor made of Hastelloy of dimensions 12 mm internal diameter and length 40 cm. The catalyst was maintained in position in the centre of the reactor using quartz wall plugs with inert packing material above and below the catalyst bed. The apparatus was then pressure-tested at 20 bar with helium to check for leaks. The catalyst was then activated by heating to 220°C at 5°C/min in helium at 16 bar for 1 hour, to ensure full decomposition of catalyst precursors.

The required flows of ethane, ethylene, 20 % oxygen in helium and water were then introduced to the reactor, to ensure the required inlet composition. This composition was 52 % v/v ethane, 6.7 % v/v oxygen, 10 % v/v ethylene, 5 % v/v water and balance helium. The total feed flow rate was maintained at a level to ensure a feed GHSV of 2000-9000/h. After equilibrating for 60 minutes, gas samples were taken from the outlet stream to a GC system (model Unicam 4400) to quantify ethane, ethylene, oxygen and helium.

The setpoint temperature of the reactor was increased to 293°C, to achieve a similar reactor temperature of 299-301°C for each of catalysts A-J, in order to facilitate direct comparison. Following a further equilibration period of 60 minutes, liquid product collection was commenced and continued for a period of typically 18 hours. During the run period, the effluent gas composition was measured using GC analysis (ProGC, Unicam). Exit gas volume was measured over the run period by a water-gas meter. The liquid products were collected and weighed after the run period. Composition of the liquid products was measured using gas chromatography analysis (Unicam 4400 and 4200 fitted with TCD and FID detectors respectively).

From analysis of the feed and product flow rates and compositions the following parameters were calculated:

25 <u>Conversions</u>:

5

10

15

20

30

of ethane = (inlet mol ethane - outlet mol ethane) / inlet mol ethane * 100 of oxygen = (inlet mol oxygen - outlet mol oxygen)/inlet mol oxygen * 100 Selectivities:

to acetic acid (C-mol %) = (outlet mol acetic acid * 2) / ((outlet mol ethylene * 2 - inlet mol ethylene * 2) + outlet mol CO + outlet mol CO₂ + outlet mol acetic acid * 2) * 100

to ethylene(C-mol %) = (outlet mol ethylene * 2)/ ((outlet mol ethylene * 2 - inlet mol

ethylene * 2) + outlet mol CO + outlet mol CO₂ + outlet mol acetic acid * 2) * 100 to CO (C-mol %) = (outlet mol CO) / ((outlet mol ethylene * 2 - inlet mol ethylene * 2) + outlet mol CO + outlet mol CO₂ + outlet mol acetic acid * 2)* 100 to CO₂ (C-mol %) = (outlet mol CO₂) / ((outlet mol ethylene * 2 - inlet mol ethylene * 2) + outlet mol CO + outlet mol CO₂ + outlet mol acetic acid * 2) * 100 to CO_x = selectivity to CO (C-mol %) + selectivity to CO₂ (C-mol %)

STY (space time yield)% = (g acetic acid)/kg catalyst bed /hour

Typically, mass balance and carbon balance for a reaction was found to be $100 \cdot +/-5 \%$.

10 Experiment A and Examples 1 to 9

5

Each catalyst A to J was employed in the general reaction method described above. The results are given in Tables 1. Each catalyst was evaluated under standard conditions indicated in Table 1.

Table 1

Experiment	Catalyst	Ethane	Sel. Acetic	Sel. C ₂ H ₄		STY AcOH
,		Convn	acid	% C-mol	% C-mol	g/kg-cat/h
		% C-	% C-mol			
		mol				
A	A	7.8	47.0	34.4	18.5	163
Example 1	В	4.2	71.3	0.0	28.7	118
Example 2	С	3.8	70.8	0.0	29.2	105
Example 3	D	6.3	56.9	24.7	18.5	133.6
Example 4	E	4.1	58.4	12.9	28.7	85.9
Example 5	F	5.1	59.9	12.6	27.4	112.7
Example 6	G	3.1	63.4	1.7	34.9	99.8
Example 7	Н	4.7	68.1	5.6	26.4	119.3
Example 8	I	5.0	70.1	5.7	24.2	131.1
Example 9	J	5.8	53.9	27.5	18.7	115.8

15 Conditions:

20

52 % v/v ethane, 6.7% v/v oxygen, 10% v/v ethylene, 5 % v/v water , balance helium. $GHSV = 3200 \, h^{-1}$; 16 bar

The results in Table 1 clearly demonstrate that compared to the comparison catalyst, catalyst A, the catalysts of the present invention achieve higher selectivities to acetic acid. Furthermore, a high selectivity to acetic acid is achieved in combination with reduced selectivity to ethylene.

Claims:

15

1. A catalyst composition for the selective oxidation of ethane to acetic acid and/or for the selective oxidation of ethylene to acetic acid which composition comprises in combination with oxygen the elements molybdenum, vanadium, niobium, gold in the absence of palladium according to the empirical formula:

 $5 Mo_a W_b A u_c V_d N b_e Z_f (I)$

wherein Z is one or more elements selected from the group consisting of B, Al, Ga, In, Ge, Sn, Pb, Sb, Cu, Pt, Ag, Fe and Re;

a, b, c, d, e and f represent the gram atom ratios of the elements such that :

$$0 < a \le 1; \ 0 \le b < 1 \text{ and } a + b = 1;$$

$$10 \qquad 10^{-5} < c \le 0.02;$$

$$0 < d \le 2;$$

$$0 < e \le 1; \text{ and}$$

$$0.0001 \le f \le 0.05$$

- 2. A catalyst composition as claimed in claim 1 wherein $0.01 < a \le 1$, $0.1 < d \le 2$, $0.01 < e \le 0.5$ and $0.0005 \le f \le 0.02$.
- 3. A catalyst composition as claimed in any preceding claim wherein Z is Sn, Ag, Fe or Re.
- 4. A catalyst composition as claimed in claim 3 wherein Z is Sn.
- 5. A catalyst composition as claimed claim 4 wherein formula I is selected from the group consisting of Mo_aW_bAu_cV_dNb_eSn_f and Mo_aAu_cV_dNb_eSn_f.
 - 6. A catalyst composition as claimed in claim 1 having the formula selected from the group consisting of $Mo_{1.000}$ $V_{0.423}$ $Nb_{0.115}$ $Au_{0.008}$ $Ag_{0.008}$ O_y , $Mo_{1.000}$ $V_{0.423}$ $Nb_{0.115}$

Au_{0.008} Fe_{0.0156} O_y, Mo_{1.000} V_{0.423} Nb_{0.115} Au_{0.008} Re_{0.008} O_y, Mo_{1.00}V_{0.423}Nb_{0.115} Au_{0.0008} Sn_{0.0008} O_y, and Mo_{1.00}V_{0.423}Nb_{0.117}Au_{0.0008} Sn_{0.0156} O_y, wherein y is a number which satisfies the valencies of the elements in the composition for oxygen.

- 7. A process for the production of acetic acid from a gaseous mixture comprising ethane and/or ethylene which process comprises contacting the gaseous mixture with a molecular oxygen-containing gas at elevated temperature in the presence of a catalyst composition as claimed in any one of the preceding claims.
 - 8. A process as claimed in claim 7 in which ethane and optionally ethylene is oxidised to a mixture comprising acetic acid.
- 10 9. A process as claimed in claim 7 or claim 8 in which the elevated temperature is in the range from 200 to 500°C.
 - 10. A process as claimed in any one of claims 7 to 9 in which the pressure is the range from 1 to 50 bar.
 - 11. A process as claimed in any one of claims 7 to 10 in which the selectivity of the oxidation reaction of ethane and/or ethylene to acetic acid is at least 50mol%.
 - 12. A process as claimed in claim 11 in which the selectivity of the oxidation reaction of ethane and/or ethylene to acetic acid is at least 60mol%.

20

15

5

25

30

A. CLASSIFICATION OF SUBJECT MATTER IPC 7 B01J23/68 B01J23/52

2 C07C51/25

C07C51/215

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) IPC 7-801J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ, INSPEC, COMPENDEX

C. DOCUM	ENTS CONSIDERED TO BE RELEVANT	
Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Х	EP 1 043 064 A (BP CHEM INT LTD) 11 October 2000 (2000-10-11) cited in the application paragraphs '0011!,'0022!,'0028!,'0029! example 1	1-12
X	WO 99 51339 A (JONES MICHAEL DAVID; KITCHEN SIMON JAMES (GB); COOK JOHN (GB); ELL) 14 October 1999 (1999-10-14) page 4, line 13 -page 5, line 13 page 6, line 11 - line 31	1,3,7-12
E	EP 1 192 987 A (ROHM & HAAS) 3 April 2002 (2002-04-03) paragraph '0024!; examples 12-14/	1

X Further documents are listed in the continuation of box C.	χ Patent family members are listed in annex.				
 Special categories of cited documents: 'A' document defining the general state of the art which is not considered to be of particular relevance 'E' earlier document but published on or after the international filing date 'L' document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) 'O' document referring to an oral disclosure, use, exhibition or other means 'P' document published prior to the international filing date but later than the priority date claimed 	 'T' later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention 'X' document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone 'Y' document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art. '&' document member of the same patent family 				
Date of the actual completion of the international search 28 November 2002	Date of mailing of the international search report 05/12/2002				
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Authorized officer Besselmann, S				

PCT/GB 02/04018

	TO BE DELEVANT	PC1/GB 02/04018			
	tion) DOCUMENTS CONSIDERED TO BE RELEVANT	Relevant to claim No.			
ategory °	Citation of document, with indication, where appropriate, of the relevant passages		riciolani to ciam 140.		
	US 6 274 765 B1 (ROESKY RANIER ET AL) 14 August 2001 (2001-08-14) the whole document				
			·		

Information on patent family members

PCT/GB 02/04018

				' `	,, ub	
Patent document cited in search report		Publication date		Patent family member(s)		Publication date
EP 1043064	А	11-10-2000	BR CN EP JP NO SG TR TW US	0001460 A 1269259 A 1043064 A 2000312826 A 20001678 A 84569 A 200000876 A 476666 E 6333444 E	4 42 4 41 41 42 3	16-01-2001 11-10-2000 11-10-2000 14-11-2000 02-10-2000 20-11-2001 21-11-2000 21-02-2002 25-12-2001
WO 9951339	A	14-10-1999	AU BR CN EP WO JP NO TR US	3160899 A 9909164 A 1303320 T 1069945 A 9951339 A 2002510543 T 20004909 A 200002817 T 6350716 B	A T A1 A1 T A	25-10-1999 16-10-2001 11-07-2001 24-01-2001 14-10-1999 09-04-2002 17-11-2000 21-12-2000 26-02-2002
EP 1192987	A	03-04-2002	US CN EP JP BR	2002065431 / 1347756 / 1192987 / 2002177784 / 0104285 /	4 41 4	30-05-2002 08-05-2002 03-04-2002 25-06-2002 07-05-2002
US 6274765	B1	14-08-2001	DE CN DE WO EP ES JP NO		B D1 A1 A1 T3	29-10-1998 11-09-2002 21-03-2002 29-10-1998 16-02-2000 16-09-2002 27-11-2001 18-10-1999